

# Factsheet: Modelling of explosion loading

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# Background/Introduction

- According to the Memorandum of Understanding, the Activity 4 of COST TU0601 concerns the engineering modelling of relevant exposures.
- The task includes the modelling and assessment of the probabilistic characteristics of extreme exposure events in the first place.
- In addition one needs information on other (normal) loads and structural properties as they determine to a large extent the effect of the event.

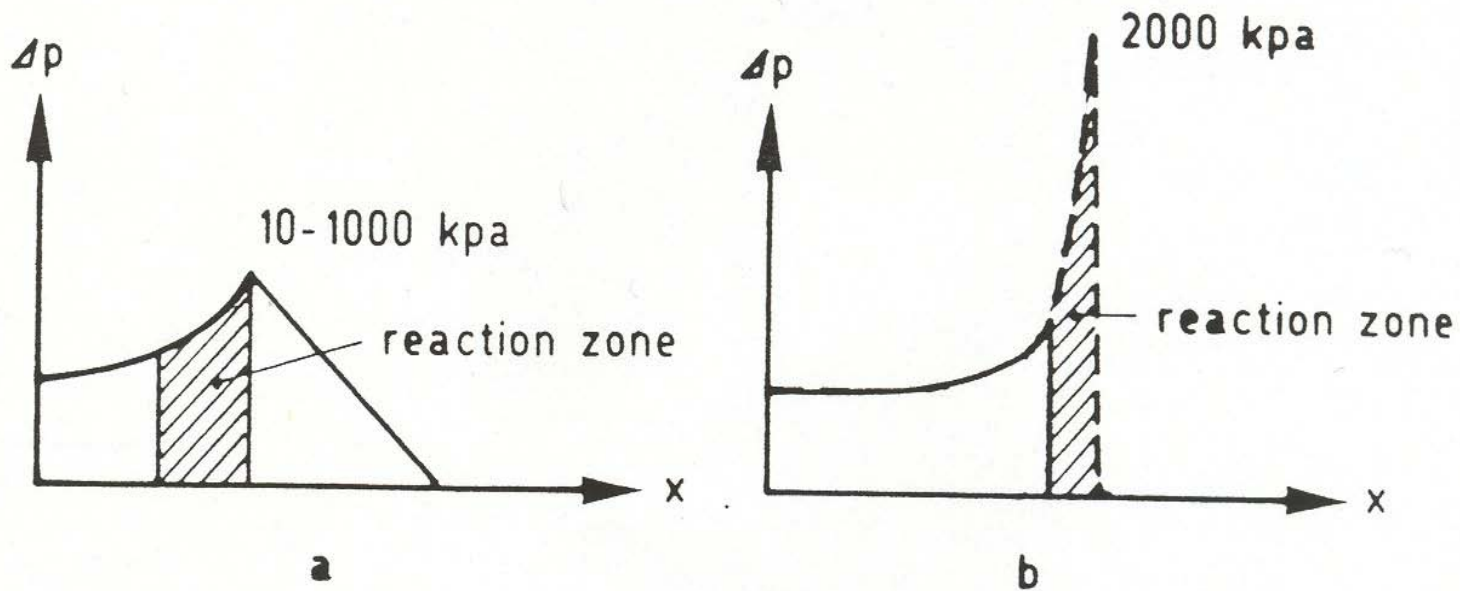
# Problem statement / Key issues

- Explosions account for a substantial number of accidental actions in buildings.
- For adequate design a model for in particular internal gas or dust explosions is wanted.
- However, literature from a structural perspective is scarce as well as the number of interested experts. The note is an attempt to bring together some material.

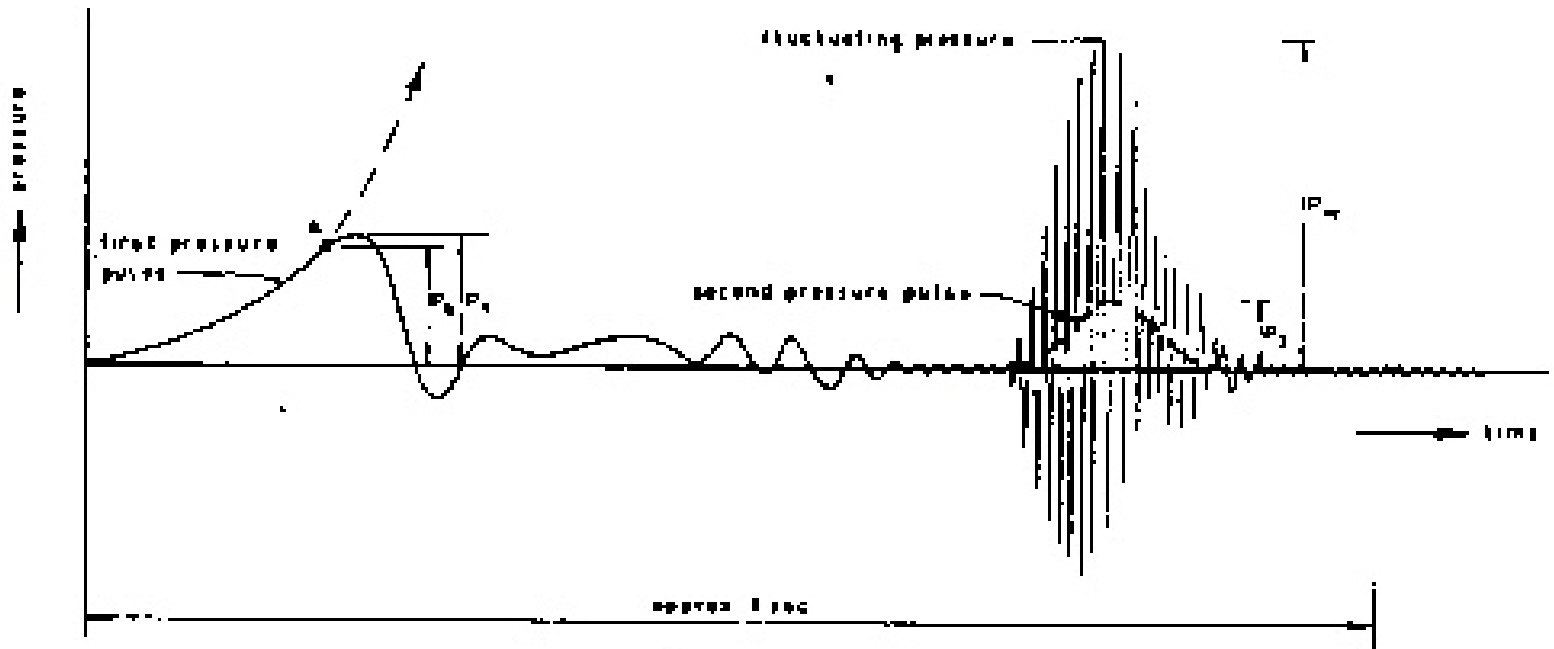
# Methodology

- Description of phenomenon
  - Detonation
  - Deflagration
  - Pressure/time variation
- Methods for prediction of loads due to internal explosions
  - Empirical and codified models
  - Phenomenological models
  - CFD-models
- Statistics
- Probability of exceedance curves

# Deflagration(left)/detonation(right)



# Pressure-time variation

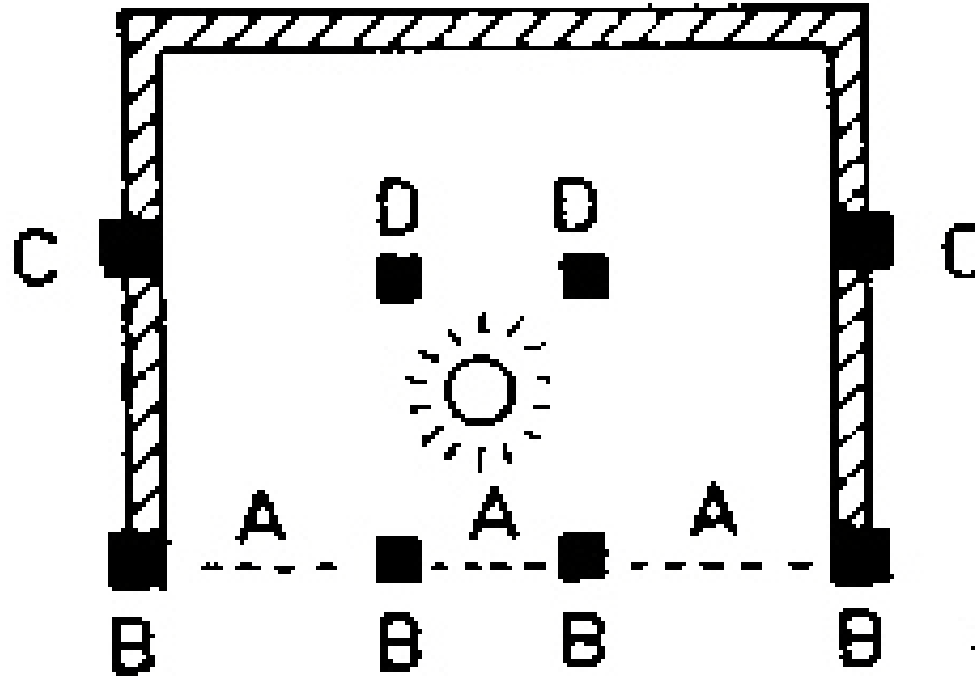


# Empirical and codified models

(further described in Annex A)

- Eurocode model
- Cubbage and Simmonds
- Rasbash et al
- NFPA-1
- NFPA-2
- Based on concept of a vent coefficient  $K_K = \frac{A_s}{A_v}$

# Configuration-dependent loading





# Phenomenological models

- Based on 1D considerations
- Trying to model some of the physics involved in the process
- Input will be a rough geometry model
- For each submodule, the blocking effect will have to be estimated
- High uncertainty should be expected for such applications
- Such models can be considered just as CFD-models with a very coarse (poor) grid resolution
- Computed pressures will be the average over a large volume
- No local pressure peaks will be picked up
- Validation of these models will generally be through comparison of simulation results with experiments

# CFD models

- Attempt to resolve the physics numerically by dividing space into small boxes (control volumes)
- Implements models for various phenomena like fluid flow and turbulence
- In each cell, all variables are assumed constant in one time step, and are based on the flow balance and fluxes
- For explosions, additional models will have to be incorporated compared to a standard CFD-model, as flame propagation and combustion will have to be modelled
- For each time step, equations for the following are solved for:
  - Mass balance (continuity)
  - Impulses
  - Entalpy
  - Turbulence
  - Fuel transport and mixture fraction.

# CFD models, contd.

- If only blast pressures in the far field are to be assessed, simplified models may be used
- Special purpose CFD-models, like FLACS, EXSIM and Auto Reagas have a greater potential to perform well. (Developed by people doing experimental and theoretical work within gas explosions)
- Still, significant differences will be seen between the models, both with regard to applicability and validity
- Geometries can be either defined by hand or imported from CAD systems

# Limitations of CFD models:

- Available computation power limiting the numerical resolution that can practically be used
- Accuracy of numerical models
- The underlying empirical sub models for
  - Reaction zone
  - Turbulence generation
  - Turbulence length scale
  - Turbulent combustion

# Observations related to application of different types of models:

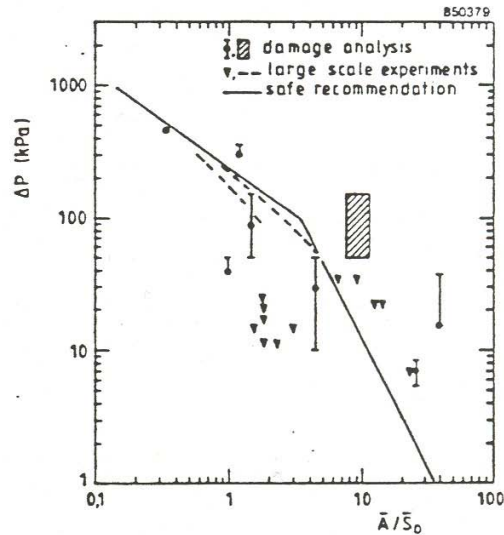
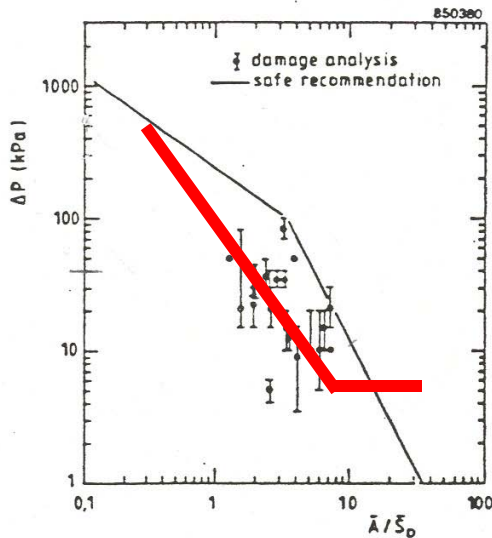
- The phenomenological code SCOPE and 'simple' CFD codes FLACS, AutoReaGas, and EXSIM are in widespread use
- Phenomenological and CFD methods generally give fairly good accuracy (within an factor of two) so these models yield solutions that are approximately correct
- The limitations associated with empirical and phenomenological methods (simplified physics and relatively crude representation of geometry) can only be overcome through additional calibration
- It is recommended to develop 'advanced' CFD codes that will allow fully realistic combustion models and resolution of all obstacles
- However it is likely to be many years before such tools are available. (This is primarily due to the large computational expense of this type of model)

# Statistics/Probabilistic modelling:

- As a function of time the ***occurrence of an explosion*** can be considered as a Poisson process
- The next step is to model the ***magnitude of the explosion***, conditional upon occurrence
- For internal explosions the maximum pressure can be taken as the maximum of the "breaking pressure" and the "vent controlled pressure"

# Statistics/Probabilistic modelling:

- The "vent control pressure" as observed in practice can be estimated from Figure 3 (The Eurocode line may be considered as an average and the coefficient of variation is about 0,7)



# Statistics/Probabilistic modelling:

- The magnitude of the overpressure, depend on many factors and data parameters, deterministic and random (see Annex A)
- Some of them are common with the probabilistic model of the fuel concentration, while others are not
- Depending on the desired accuracy of probabilistic model, random parameters can be represented by random variables, random processes (in time) and random fields (in space and time)



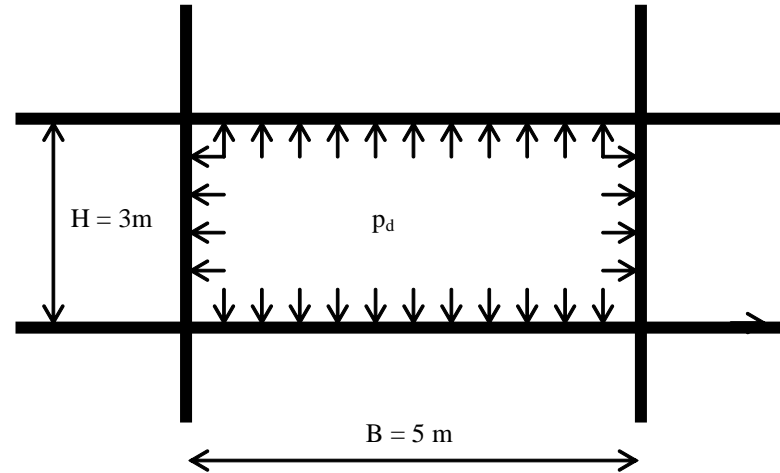
# Statistics/Probabilistic modelling:

- Four natural sub-algorithms for calculation of explosion loads:
  - Estimation of probability model for fuel concentration due to gas dispersion at one leak area
  - Estimation of the probability distribution function for ignition events
  - Estimation of the probability distribution function for ignition events
  - Estimation of gas explosion overpressure for a given homogeneous cloud made of flammable fuel-air mixture

# Probability of exceedance curves:

- 3D-surfaces plotting probability of exceeding both a pressure level and an impulse level can be useful for a simplistic structural assessment.
- When numerical methods are applied, other model uncertainty factors will clearly be relevant as compared to the analytical approach (i.e. simplified empirical models)
- For quantification of the model uncertainty related to numerical models, it is referred to some recent publications

# Example / Illustration / Case studies



V	Volume	180 m <sup>3</sup>
As	Area of side of enclosure	200 m <sup>2</sup>
Av/V	Vent area parameter	0.01 - 0.20 m <sup>-1</sup>
p <sub>v</sub>	Vent breaking pressure	3 kN/m <sup>2</sup>
S <sub>o</sub>	Burning velocity	0.45 m/s
W	Mass density of vent material	20 kg/m <sup>2</sup>

# Comparison of empirical models

			$Av/V [m^{-1}]$	$Av [m^2]$	K	EN kN/m <sup>2</sup>	cubbage kN/m <sup>2</sup>	rasbash kN/m <sup>2</sup>	nfa kN/m <sup>2</sup>
			0,01	1,60	125,00	404,50	89,49	534,11	3125,00
V	160	m3	0,02	3,20	62,50	104,50	44,86	269,42	781,25
As	200	m2	0,03	4,80	41,67	48,94	29,99	181,20	347,22
pv	3	kN/m2	0,04	6,40	31,25	29,50	22,55	137,08	195,31
So	0,45	m/s	0,05	8,00	25,00	20,50	18,08	110,61	125,00
W	20	kg/m2	0,06	9,60	20,83	15,61	15,11	92,97	86,81
			0,07	11,20	17,86	12,66	12,98	80,36	63,78
			0,08	12,80	15,63	10,75	11,39	70,91	48,83
			0,09	14,40	13,89	9,44	10,15	63,56	38,58
			0,10	16,00	12,50	8,50	9,16	57,67	31,25
			0,11	17,60	11,36	7,81	8,35	52,86	25,83
			0,12	19,20	10,42	7,28	7,67	48,85	21,70
			0,13	20,80	9,62	6,87	7,10	45,46	18,49
			0,14	22,40	8,93	6,54	6,61	42,55	15,94
			0,15	24,00	8,33	6,28	6,18	40,03	13,89
			0,16	25,60	7,81	6,06	5,81	37,82	12,21
			0,17	27,20	7,35	5,88	5,48	35,88	10,81
			0,18	28,80	6,94	5,73	5,19	34,15	9,65
			0,19	30,40	6,58	5,61	4,93	32,60	8,66
			0,20	32,00	6,25	5,50	4,70	31,20	7,81
			0,21	33,60	5,95	5,41	4,48	29,94	7,09
			0,22	35,20	5,68	5,33	4,29	28,80	6,46
			0,23	36,80	5,43	5,26	4,11	27,75	5,91
			0,24	38,40	5,21	5,19	3,95	26,79	5,43
			0,25	40,00	5,00	5,14	3,80	25,91	5,00

# Annex A: Description of models

*(1) Eurocode EN 1991-1-7*

*(2) Cabbage and Simmonds*

*(3) Rasbash et al*

*(4) NFPA 68, Guide for Venting of Deflagrations, 2002 Edition for low strength buildings*

*(5) NFPA 68, Guide for Venting of Deflagrations, 2002 Edition for high strength buildings*

# Annex B: Table CFD parameters

Deterministic factors	Random factors
type of problem: e.g. gas explosion in vessels, gas explosion in buildings / off- shore modules, gas explosion in uncon- fined process areas	position of leakage points. (They can be even deterministic with different proba- bilities of gas dispersion events.)
shape and sizes of structure / processing area	flow rate of gas/liquid
shape, location and sizes of equipment	wind direction and velocity
type of fuel and oxidiser	air exchange rate due to natural ventila- tion [and forced ventilation
size, location and type of explosion vent area	ignition source: strength and position
mitigation system	time to ignition: time delay after gas has been released
minimum ignition energy as a function of fuel concentration	temperature field
autoignition temperature	
flammability limits (in terms of fuel-air concentration) as a function of tempera ture	
stoichiometric composition, which gives usually the highest explosion pressure	

# Additional items, not completed

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## Limitations

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## Recommendations

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## Outlook to further research

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- Accuracy vs. Computation time

- Various types of models can be applied for different purposes

- Further work on more comprehensive CFD models

- Continuous need for calibration of models by experimental results

- Further work on probabilistic modelling